

Turbulent portion of the boundary layer

In turbulent boundary layer neglect the existence of buffer layer. The region near to the surface is laminar sub-layer this region is assumed to be neglected. So that the motion is effected entering by eddy motion. Assumed that the shear stress at a plane surface can be calculated from the expression developed by Blasius:

$$\frac{R}{\rho u_s^2} = 0.228 \left(\frac{\mu}{\rho \delta u_s} \right)^{0.25} \quad (11)$$

δ : thickness of boundary layer developed by Blasius using power law $\frac{u_x}{u_s} = \left(\frac{y}{\delta} \right)^f$ (12)

By substitute for value of the $u_s = u_x \left(\frac{y}{\delta} \right)^f$ in equation (12) into equation (11):

$$R = 0.0228 \rho^{0.75} \mu^{0.25} \delta^{-0.25} u_x^{1.75} \left(\frac{\delta}{y} \right)^{1.75f}$$

By using dimension analysis [$0 = -0.25 + 1.75f$] the $f = \frac{1}{7}$

$$\frac{u_x}{u_s} = \left(\frac{y}{\delta} \right)^{\frac{1}{7}} \quad (13)$$

Assumptions: known as Prandtl seventh law which is used to calculate the turbulent boundary layer

Through using equation 13 and combined with equation (2) we can get:

$$\frac{\partial}{\partial x} \int_0^l \rho (u_s - u_x) u_x dy = -R_o \quad (2)$$

$$u_x = u_s \left(\frac{y}{\delta}\right)^{\frac{1}{7}} \quad (13)$$

$$\begin{aligned} \int_0^l (u_s - u_x) u_x dy &= \int_0^\delta u_s^2 \left(1 - \left(\frac{y}{\delta}\right)^{\frac{1}{7}}\right) \left(\frac{y}{\delta}\right)^{\frac{1}{7}} dy + \int_\delta^l (u_s - u_s) \cdot u_s dy \\ &= u_s^2 \int_0^\delta \left(\frac{y}{\delta}\right)^{\frac{1}{7}} - \left(\frac{y}{\delta}\right)^{\frac{2}{7}} dy = u_s^2 \delta \left(\frac{7}{8} - \frac{7}{9}\right) \end{aligned}$$

$$\int_0^l (u_s - u_x) u_x dy = \frac{7}{72} u_s^2 \delta \quad 14$$

Substitute equation (14) and equation (11) in equation (2):

$$\rho \frac{\partial}{\partial x} \left(\frac{7}{72} u_s^2 \delta \right) = 0.228 \rho u_s^2 \left(\frac{\mu}{\rho \delta u_s} \right)^{0.25}$$

$$\frac{\delta}{x} = \mathbf{0.376 Re_x^{-0.2}} \quad 14 \quad \text{For turbulent local thickness}$$

δ : include laminar and buffer layer (laminar sub-layer is vary thin) so the velocity is constant .

Laminar sub- layer

Assume at $x=x$ the laminar sub-layer is of thickness δ_b and the total thickness of the boundary layer is (δ) . Since the laminar sub-layer is very thin so the velocity gradient and shear stress are *constant* inside this layer

$$R_o = -\mu \left(\frac{\partial u_x}{\partial y} \right)_{y=0} = -\mu \frac{u_x}{y} \quad 15$$

Where $y = \delta_b$

By substitute equation 15 into equation 11

$$\mu \frac{u_x}{y} = 0.0228 \rho u_s^2 \left(\frac{\mu}{\rho \delta u_s} \right)^{0.25}$$

$$u_x = 0.0228 \rho u_s^2 \frac{y}{\mu} \left(\frac{\mu}{\rho \delta u_s} \right)^{0.25}$$

At the leading edge $u_x = u_b$ and $y = \delta_b$

$$u_b = 0.0228 \rho u_s^2 \frac{\delta_b}{\mu} \left(\frac{\mu}{\rho \delta u_s} \right)^{0.25}$$

$$= 0.0228 \rho u_s^2 \frac{\delta_b}{\mu} \left(\frac{\mu}{\rho \delta u_s} \right)^1 \left(\frac{\mu}{\rho \delta u_s} \right)^{-3/4}$$

$$\frac{\delta_b}{\delta} = \frac{1}{0.0228} \left(\frac{u_b}{u_s} \right) \left(\frac{\mu}{\rho u_s \delta} \right)^{-3/4} \quad 16$$

This equation represents the thickness ratio of sub-layer to turbulent boundary layer.

At the leading edge of the laminar sub-layer:

from equation (13) $\frac{u_b}{u_s} = \left(\frac{\delta_b}{\delta} \right)^{1/7}$ (13b) with re-arrange, then substitute in equation (16)

$$\left(\frac{u_b}{u_s}\right)^7 = \frac{1}{0.0228} \left(\frac{u_b}{u_s}\right) \left(\frac{\mu}{\rho u_s \delta}\right)^{-3/4} \quad (X^7 / X = A y^{-3/4})$$

$$\frac{u_b}{u_s} = 1.87 Re_\delta^{-1/8} \quad (17)$$

Where $Re_\delta = \frac{u_s \rho \delta}{\mu}$ and δ is the thickness of turbulent layer

The thickness in fully turbulent layer is given by equation $\frac{\delta}{x} = 0.376 Re_x^{-0.2}$ therefore from this equation :

$$\delta = 0.376 x^{0.8} \left(\frac{\mu}{\rho u_s}\right)^{0.2} \quad (18)$$

Substitute the equation (18) in equation (17) to get:

$$\frac{u_b}{u_s} = 1.87 \left[\frac{u_s \rho}{\mu} 0.376 \frac{x^{0.8} \mu^{0.2}}{u_s^{0.2} \rho^{0.2}} \right]^{-1/8} \quad (19)$$

$$\frac{u_b}{u_s} = 2.11 Re_x^{-0.1} \quad (20)$$

Notes

$Re_x = \frac{u_s \rho x}{\mu}$, where x is the distance of flow, u_s is the mainstream velocity (constant), u_b is the velocity inside the laminar sub-layer.

If the **thickness** is given in question, then use the equation (17), but if the **distance** is given (20) is used.

From equations: (13b, 18, and 20) for δ :

$$\frac{\delta_b}{\delta} = \left(\frac{u_b}{u_s}\right)^7 = \frac{190}{Re_x^{0.7}}$$

$$\frac{\delta_b}{x} = \frac{190}{Re_x^{0.7}} \cdot \frac{0.376}{Re_x^{0.2}}$$

$$\frac{\delta_b}{x} = 71.5 Re_x^{-0.9} \quad (21) \quad \text{for thickness calculating}$$

Shear stress at the surface, at a distance (x) from the leading edge is $= \mu \frac{u_b}{\delta_b}$, - $R = R_b$

Substitute for u_b equation (20) and δ_b equation (21)

$$\frac{R}{\rho u_s^2} = 0.0296 Re_x^{-0.2} \quad (22) \text{ for local friction factor}$$

The mean value of $\frac{R}{\rho u_s^2}$ over the range of $x = 0$ to $x = x$ substitute in equation (22)

$$\left(\frac{R}{\rho u_s^2}\right)_{\text{mean}} \times x = \int_0^x \left(\frac{R}{\rho u_s^2}\right) dx = \int_0^x 0.0296 Re_x^{-0.2} dx$$

$$\left(\frac{R}{\rho u_s^2}\right)_{\text{mean}} = 0.037 Re_x^{-0.2} \quad (23)$$

Mean friction force in laminar sub-layer for $x = 0$ to $x = x$

The total shear force acting on the surface is found by adding the forces acting in the streamline ($x < x_c$) [where x_c : is the critical distance between the streamline and turbulent regions] and turbulent region ($x > x_c$), this can be done by providing the critical value of Re_x .

Where:

In streamline,
$$\frac{R}{\rho u_s^2} = 0.646 Re_x^{-0.5}$$

And for turbulent
$$\left(\frac{R}{\rho u_s^2}\right)_{\text{mean}} = 0.037 Re_x^{-0.2}$$

❖ In calculating the mean value of $\left(\frac{R}{\rho u_s^2}\right)_{\text{mean}}$ in turbulent region it was assume that the turbulent layer extended to leading edge. A more accurate value of mean value of $\left(\frac{R}{\rho u_s^2}\right)_{\text{mean}}$ over the whole surface can be obtained by using the expression for laminar condition from $x = 0$ to $x = x_c$ and for turbulent from $x = x_c$ to $x = x$ therefore the mean value:

❖
$$\left(\frac{R}{\rho u_s^2}\right)_{\text{mean}} = \frac{1}{x} [0.646 Re_x^{-0.5} \cdot x_c + 0.037 Re_x^{-0.2} x - 0.037 Re_{x_c}^{-0.2} \cdot x_c]$$

❖
$$= 0.037 Re_x^{-0.2} + Re_x^{-1} [0.646 Re_{x_c}^{0.5} - 0.037 Re_{x_c}^{0.8}] \quad (24)$$

Note

The change from streamline to turbulent conditions in the boundary layer occurs at a certain critical distance from the leading edge . This distance depends on the shape of leading edge .For a given surface the transition takes place at critical value of Reynold number, the critical Re_{x_c} at $(x_c) = 10^5$ at the surface .

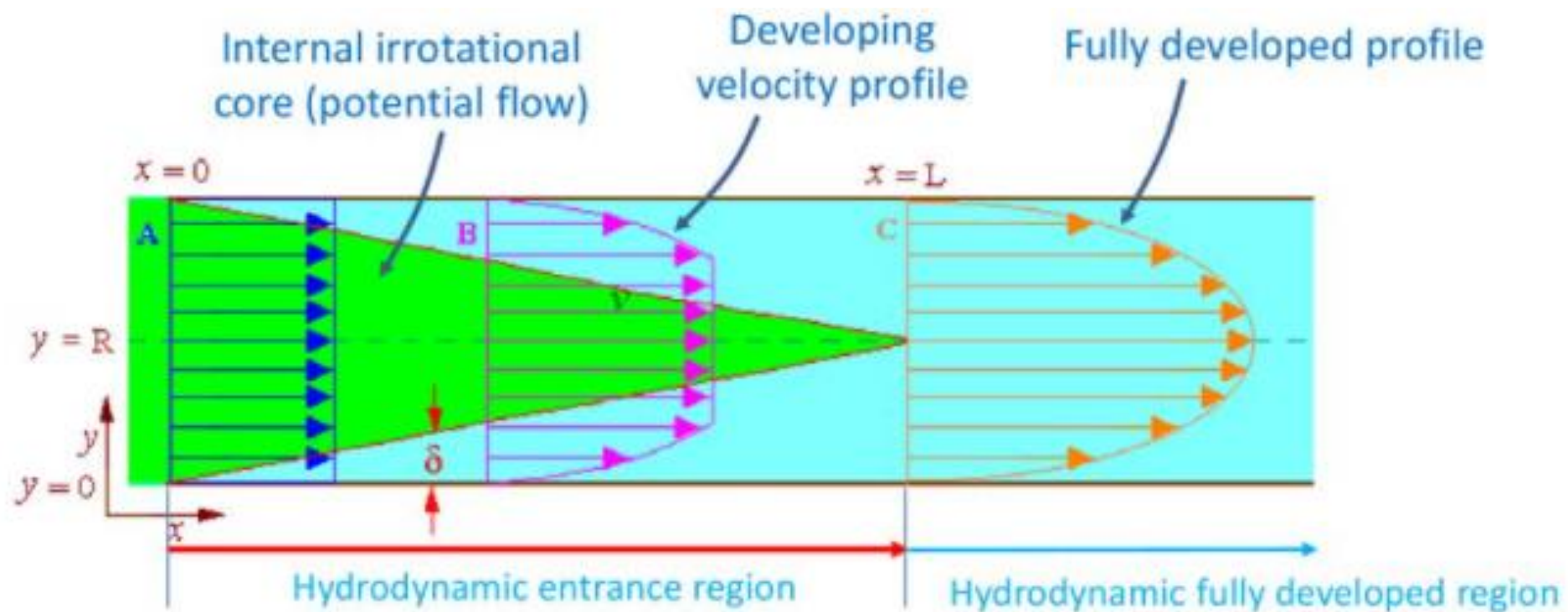
Application of boundary layer theory through a pipe flow :-

Consider a fluid entering a circular pipe at a uniform velocity (fig. in next. slide). Because of the no-slip condition, the fluid particles in the layer in contact with the surface of the pipe come to a complete stop. This layer also causes the fluid particles in the adjacent layers to slow down gradually as a result of friction. The region of the flow in which the effects of the viscous shearing forces caused by fluid viscosity are occurred, is called as the velocity boundary layer or just the boundary layer.

$$u_x = u_s \left(\frac{y}{r}\right)^{\frac{1}{7}} \quad \text{where } u_s = \text{velocity at the center, maximum velocity.}$$

Shear stress at the walls is given by the Blasius equation.

$$\frac{R}{\rho u_s^2} = 0.0228 \left(\frac{\mu}{\rho u_s r}\right)^{\frac{1}{4}} \quad \text{substitute } u = 0.82u_s , d = 2r$$



δ = Boundary layer thickness
 R = Radius of pipe
 L = Transition length
 v = Velocity

Potential flow regime

Boundary layer flow

Development of boundary-layer flow in pipe

$$\frac{R}{\rho u^2} = 0.0384 Re^{-\frac{1}{4}} \quad (25) \quad \text{for turbulent} \quad Re = \frac{u \rho d}{\mu}$$

The velocity at the edge of laminar sub-layer is $\frac{u_b}{u_s} = 1.87 \left(\frac{\mu}{\rho u_s r} \right)^{\frac{1}{8}}$

$$\frac{u_b}{u_s} = 2.49 Re^{-\frac{1}{8}} \quad (26) \quad Re = \frac{u \rho d}{\mu}$$

The thickness of laminar sub-layer:

$$\frac{\delta_b}{r} = \left(\frac{u_b}{u_s} \right)^7 = (1.78)^7 \left(\frac{\mu}{\rho u_s r} \right)^{\frac{7}{8}}$$

$$\frac{\delta_b}{d} = 62 Re^{-7/8} \quad (29)$$

Summary

- Laminar boundary layer:

- $\frac{\delta}{x} = 4.64 Re_x^{-1/2}$ (8) {velocity profile is polynomial series}. To find the thickness

- $\frac{R_o}{\rho u_s^2} = -0.323 Re^{-1/2}$ (9) To find shear stress

Turbulent boundary layer

- ❖ $\frac{\delta}{x} = 0.376 Re_x^{-0.2}$ 14 For turbulent fully developed flow (neglect laminar sub-layer)

- ❖ $\frac{R}{\rho u_s^2} = 0.228 Re_\delta^{-0.25}$

Laminar sub-layer:

To find velocity in presence laminar sublayer:

$$\square \frac{u_b}{u_s} = 1.87 Re_\delta^{-1/8} \quad (17)$$

$$\square \text{ Or } \frac{u_b}{u_s} = 2.11 Re_x^{-0.1} \quad (20)$$

$$\square \frac{\delta_b}{x} = 71.5 Re_x^{-0.9} \quad (21) \quad \text{for thickness calculating}$$

$$\square \frac{R}{\rho u_s^2} = 0.0296 Re_x^{-0.2} \quad (22) \quad \text{for local friction factor}$$

$$\square \left(\frac{R}{\rho u_s^2} \right)_{\text{mean}} = 0.037 Re_x^{-0.2} \quad (23)$$

HW

Calculate the thickness of the boundary layer at a distance of 75 mm from the leading edge of a plane surface over which water is flowing at a rate of 3 m/s. Assume that the flow in the boundary layer is streamline and that the velocity u of the fluid at a distance y from the surface can be represented by the relation $u = a + by + cy^2 + dy^3$, where the coefficients a , b , c , and d are independent of y . The viscosity of water is 1 mN s/m^2 .

Ans. $\delta = 0.000734 \text{ m}$ or 0.734 mm